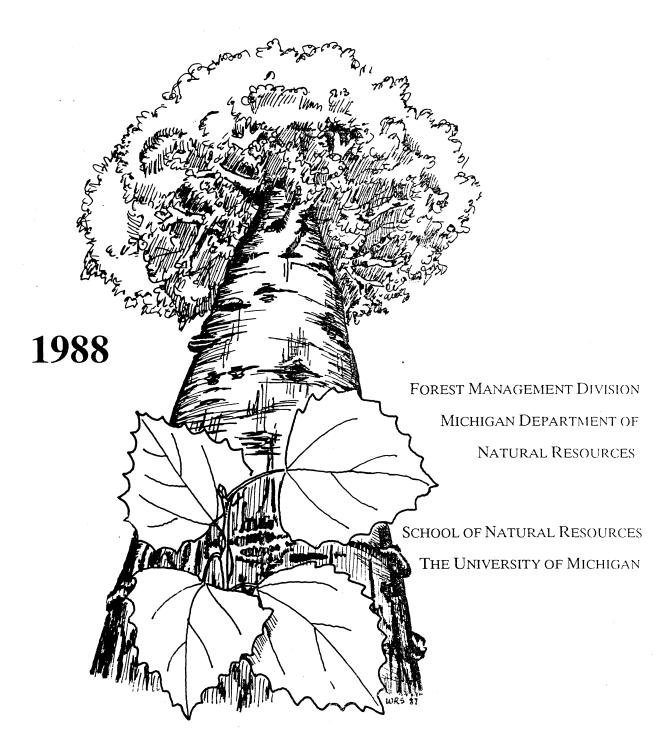
# INDIVIDUAL TREE SAWTIMBER VOLUME EQUATIONS FOR ASPEN IN MICHIGAN

BY

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## Management Summary

New cubic-foot and Doyle, International 1/4-inch, and Scribner board-foot individual tree sawtimber volume equations were developed for aspen in Michigan. Data used to develop these equations were collected from 24 aspen stands in Michigan (12 stands each from the Upper and Lower Peninsulas). Four stands each were sampled from each of the six state forests in Michigan.

Examination of coefficients of determination ( $\mathbb{R}^2$ ), standard errors of the estimate ( $\mathbb{S}_{y \cdot x}$ ), and an independent validation data set for a series of linear and nonlinear regression equations indicated that nonlinear equations were most accurate for all types of volume. The new International 1/4-inch and Scribner board-foot volume equations yielded volume estimates (1) smaller than the values in Tables 1 and 2 of Gevorkiantz and Olsen (1955) for DBH's  $\geq 18$  in. with mixed results for smaller DBH's and (2) larger than the values in Tables 6 and 10 of Edminster et al. (1982) except for small merchantable heights. The new individual tree volume equations are:

1. Cubic-foot volume

$$\hat{V}_C = 0.3457 + 0.1126D^{1.513}H^{0.9467}$$

2. Doyle board-foot volume

$$\hat{V}_D = 1.311 + 0.04927D^{2.236}H^{1.101}$$

3. International 1/8-inch board-foot volume

$$\hat{V}_{I} = 3.208 + 0.4478D^{1.606}H^{1.077}$$

4. Scribner board-foot volume

$$\hat{V}_S = 2.484 + 0.3169D^{1.685}H^{1.076}$$

where D is DBH in inches and H is merchantable height in 100-in. sticks to an approximate 7.6-in. top diameter limit. International 1/4-inch volumes are obtained by multiplying 0.905 times volumes obtained from Equation 3.

Multiple linear regression equations were developed to predict (1) one type of volume from another type and (2) Doyle, International 1/4-inch, and Scribner board-foot cubic-foot ratios as a function of D, H, and D and H.

The above equations can be used to develop tables as we have done in this paper or entered into a computer program to facilitate computer volume calculations for cruise data.

# Michigan Department of Natural Resources Forest Management Division

## SUBJECT--INDIVIDUAL TREE VOLUME EQUATIONS

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TITLE

-- Individual Tree Sawtimber Volume Equations for Aspen in Michigan

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## Background

Composite individual tree sawtimber board-foot (i.e., Scribner and International 1/4-inch rules) volume tables have been developed for the Lake States by Gevorkiantz and Olsen (1955). Volume equations and tables have been developed for aspen in Colorado (Edminster et al. 1982). The tables of Gevorkiantz and Olsen or some modifications of them are still widely used in Michigan for aspen.

#### Purpose

The purpose of this paper is to present new sawtimber cubic-foot and Doyle, International 1/4-inch, and Scribner board-foot individual tree volume equations and tables for aspen in Michigan.

#### **Methods and Materials**

Felled tree and/or standing tree measurements were made on a total of 1381 trees from 24 stands as follows:

- 1) 677 trees from 12 stands in the Upper Peninsula (i.e., 4 stands each in the Copper, Escanaba River, and Lake Superior state forests), and
- 2) 704 trees from 12 stands in the Lower Peninsula (i.e., 4 stands each in the Mackinaw, Au Sable, and Marquette state forests).

Measurements were taken on 728 bigtooth aspen and 653 trembling aspen trees. Stands were selected from the six forests to roughly represent the range of site index, age, stand density, average diameter at breast height (DBH), and average height found in Michigan. Measurements were made during May through August, 1986.

For the 24 stands, site index varied from 51 to 79, age varied from 47 to 70 years, basal area/acre varied from 70 to 186 sq. ft., average DBH varied from 7.7 to 11.9 in., average total height varied from 52.2 to 77.5 ft., and average merchantable height to an approximate 3.6-in. minimum top diameter varied from 3.4 to 7.7 100-in. sticks.

For felled trees, DBH to the nearest 0.1 in., total height to the nearest ft., merchantable height to the nearest 100-in. stick to an approximate 3.6-in. minimum top diameter, and diameter inside (DIB) and outside (DOB) bark to the nearest 0.1 in. at the end of each stick were measured for each tree. For standing trees, measurements were taken at stump height (0.5 ft.), DBH height (4.5 ft.), several upper stem taper breaks, approximate 3.6-in. DIB height, and the tree top using a Barr and Stroud Dendrometer. A bark factor equation was developed using the felled tree data to estimate DIBs for standing trees (Fowler and Hussain 1987a). Fowler and Hussain (1987b) developed pulpwood, sawtimber, and residual pulpwood individual tree cubic-foot volume equations from the total data set described above.

Sawtimber trees were defined as trees that had a least one 100-in. stick with a minimum inside bark top diameter no smaller than 7.6 inches. Sawtimber merchantable height is defined as the number of 100-in. sticks that can be cut out of a tree with a minimum top diameter no smaller than 7.6 inches. There was a total of 946 sawtimber trees.

For each tree, cubic-foot volumes were calculated for each 100-in. stick using Smalian's formula. The volume of the butt stick was determined by breaking the stick into two pieces at DBH height, calculating the volume separately for each piece using

Smalian's formula, and summing the two volumes. For each 100-in. stick, cubic-foot and board-foot volumes were calculated using the following formulas:

Cubic-foot: 
$$V = \frac{(B + b)L}{2}$$
 (Avery and Burkhart 1983)

Doyle:  $V = 0.5D^2 - 4.0D + 8.0$  (Husch et al. 1982)

International 1/8-inch:  $V = 0.44D^2 - 1.20D - 0.30$  (Husch et al. 1982)

Scribner:  $V = 0.395D^2 - 0.99D - 2.15$  (Bruce and Schumacher 1950)

where

V = volume in cubic feet or board feet,

L = length of stick (100 in.) in ft.,

B = cross-sectional area inside bark of large end of the stick in sq. ft.,

b = cross-sectional area inside bark of small end of the stick in sq. ft., and

D = diameter of small end of the stick inside bark in inches.

See Avery and Burkhart (1983) and Husch et al. (1982) for detailed discussions of cubicfoot volumes and board-foot log rules.

Cubic-foot and the three board-foot volumes for each tree were determined by summing up the volumes of all sawtimber sticks to a 7.6-in. top diameter limit.

International 1/8-inch volumes were calculated for each tree, and all regression equations were developed using these volumes. International 1/4-inch volumes were obtained by multiplying 0.905 times the International 1/8-inch volumes.

Individual tree volume was regressed on various variables determined from tree DBH and merchantable height using multiple linear and nonlinear regression.

#### Results

The data set used to develop the regression equations consisted of 750 trees (? 80%) selected at random from the total of 946 trees. Fowler and Hussain (1987b) found no significant differences between pulpwood cubic-foot volume equations of the six forest areas and two species, so the data for both species and all stands were pooled

before developing volume regression equations. All equations were based on the 750 trees with an average DBH = 10.8 in. (range: 8.0 to 16.7), average merchantable height = 2.8 sticks (range: 1 to 7), average cubic-foot volume = 12.20 (range: 2.82 to 54.49), average Doyle board-foot volume = 38.73 (range: 6.48 to 262.24), average International 1/8-inch board-foot volume = 72.83 (range: 15.99 to 380.35), and average Scribner board-foot volume = 62.34 (range: 13.14 to 335.85).

## Cubic-foot and board-foot volume prediction equations

A comparison of various multiple linear regression and nonlinear regression equations based on goodness-of-fit and simplicity indicated that the following nonlinear prediction equation compared favorably to all other equations examined for cubic-foot and the three board-foot volumes:

$$\hat{\mathbf{V}} = \hat{\boldsymbol{\beta}}_{0} + \hat{\boldsymbol{\beta}}_{1} \mathbf{D}^{\hat{\boldsymbol{\beta}}_{2}} \mathbf{H}^{\hat{\boldsymbol{\beta}}_{3}}$$

 $\hat{V} = \hat{\beta}_0 + \hat{\beta}_1 D^{\hat{\beta}_2} H^{\hat{\beta}_3}$  where  $\hat{V}$  is predicted volume, D is DBH in inches, and H is merchantable height in 100-in. sticks to a 7.6-in. top diameter limit.  $\hat{\beta}_0$  is the sample intercept or regression constant, and  $\hat{\beta}_1$ ,  $\hat{\beta}_2$ , and  $\hat{\beta}_3$  are the sample regression coefficients related to the independent variables.

TABLE 1 shows the sawtimber volume prediction equations for cubic-foot and Doyle, International 1/8-inch, and Scribner board-foot volumes along with standard errors of the estimate  $(s_{y \bullet x})$ , and coefficients of determination  $(R^2)$ .

A cubic-foot volume table is shown in TABLE 2, and Doyle, International 1/4-inch, and Scribner board-foot volume tables are shown in TABLES 3, 4, and 5, respectively. The International 1/4-inch board-foot values in TABLE 4 were obtained by multiplying 0.905 times the values from Equation 3.

The values in our TABLE 4 (International 1/4-inch board-foot volumes) are smaller for lower merchantable heights and larger for higher merchantable heights compared to the values in TABLE 2 of Gevorkiantz and Olsen (1955) for DBH's less than 18 inches. The merchantable height where the values in our table become larger increases as DBH increases. For DBH's of 18 inches and over, our table, in general, gives smaller values.

TABLE 1. Estimated parameters  $(\hat{\beta}_0, \hat{\beta}_1, \hat{\beta}_2, \text{ and } \hat{\beta}_3)$ , standard errors of the estimate  $(s_{y \cdot x})$ , and coefficients of determination  $(R^2)$  for the cubic-foot and three board-foot volumes.

Prediction Equation	$\hat{m{eta}}_{\mathbf{O}}$	$\hat{\beta}_1$	$\hat{eta}_2$	$\hat{\beta}_3$	s <sub>y·x</sub>	$R^2$
(1) Cubic-foot <sup>a</sup>	0.3457	0.1126	1.513	0.9467	0.66	0.993
(2) Doyle <sup>b</sup>	1.311	0.04927	2.236	1.101	4.60	0.980
(3) International 1/8-inch <sup>c</sup>	3.208	0.4478	1.606	1.077	5.84	0.988
(4) Scribner <sup>d</sup>	2.484	0.3169	1.685	1.076	5.30	0.987

 $<sup>{}^{</sup>a}$ V = 0.3457 + 0.1126D<sup>1.513</sup>H<sup>0.9467</sup>

 $<sup>^{</sup>b}$ V = 1.311 + 0.04927D<sup>2.236</sup>H<sup>1.101</sup>

 $<sup>^{\</sup>circ}V = 3.208 + 0.4478D^{1.606}H^{1.077}$ 

 $<sup>^{\</sup>rm d}$ V = 2.484 + 0.3169D<sup>1.685</sup>H<sup>1.076</sup>

*TABLE 2.* Volume table showing cu. ft. volume for various combinations of DBH and merchantable height in sticks to an approximate 7.6" top diameter limit (Equation 1).

DBH	Merchantable Height in Sticks								
(inches)	1	2	3	4	5	6	7	8	9
9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	3.5 4.0 4.6 5.2 5.8 6.4 7.1	6.4 7.4 8.5 9.7 10.9 12.1 13.4 14.7 16.1 17.5 19.0 20.5	9.2 10.7 12.3 14.0 15.8 17.6 19.5 21.5 23.5 25.6 27.7 29.9 32.2 34.5 36.9 39.3 41.8	12.0 14.0 16.1 18.3 20.6 23.0 25.5 28.1 30.7 33.5 36.3 39.2 42.2 45.2 48.4 51.6 54.8	14.7 17.2 19.8 22.5 25.4 28.3 31.4 34.6 37.9 41.3 44.8 48.4 52.0 55.8 59.7 63.6 67.6	20.3 23.4 26.7 30.1 33.6 37.3 41.1 45.0 49.0 53.1 57.4 61.8 66.2 70.8 75.5 80.3	30.8 34.7 38.8 43.1 47.4 52.0 56.6 61.4 66.4 71.4 76.6 81.9 87.3 92.9	39.4 44.0 48.8 53.8 58.9 64.2 69.7 75.3 81.0 86.9 92.9 99.1 105.3	54.5 60.1 65.8 71.8 77.8 84.1 90.5 97.1 103.8 110.7 117.7

TABLE 3. Volume table showing Doyle bd. ft. volume for various combinations of DBH and merchantable height in sticks to an approximate 7.6" top diameter limit (Equation 2).

DBH	Merchantable Height in Sticks								
(inches)	1	2	3	4	5	6	7	8	9
9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	8 10 12 14 17 19 22	16 20 24 29 34 40 46 53 61 69 78 87	24 30 37 44 52 62 72 83 94 107 121 135 151 167 184 203 222	32 40 50 60 71 84 98 113 129 147 165 185 206 229 253 278 304	41 51 63 76 91 107 125 144 165 187 211 236 264 292 323 355 389	62 77 93 111 131 152 176 201 228 258 289 322 357 394 433 475	110 131 155 180 208 238 270 305 342 381 423 467 513 562	152 179 209 241 276 313 353 396 441 489 540 594 651	237 274 314 356 402 450 502 557 615 676 741

Volume table showing International 1/4-inch bd. ft. volume for various combinations of DBH and merchantable height in sticks to an approximate 7.6" top diameter limit (0.905 x Equation 3).

DBH	Merchantable Height in Sticks								
(inches)	1	2	3	4	5	6	7.	8	9
9	17	32	48	64	81				
10	19	37	56	76	95	116			
11 12	22	43	65	88	111	134			
12	25	49	74	100	127	154	181		
13	28	55	84	114	144	175	206	237	
14	31	62	95	128	162	196	231	267	
15	34	69	105	143	180	219	258	297	337
16		76	117	158	200	243	286	330	374
17		84	128	174	220	267	315	363	412
18		92	140	190	241	292	345	398	451
19		100 -	153	207	262	319	376	433	492
20		108	165	225	285	346	408	470	534
21			179	243	308	374	441	509	577
21 22			192	261	331	403	475	548	621
23			206	280	356	432	510	. 588	667
24 25			221	300	381	463	546	629	714
25			236	320	406	494	582	672	762

TABLE 5. Volume table showing Scribner bd. ft. volume for various combinations of DBH and merchantable height in sticks to an approximate 7.6" top diameter limit (Equation 4).

DBH	Merchantable Height in Sticks								
(inches)	1	2	3	4	5	6	7	8	9
9 10 11 12 13 14 15 16 17 18 19 20 21 22	15 18 21 23 26 30 33	30 35 40 46 53 60 67 74 82 90 98 106	44 53 61 71 80 91 102 113 125 137 150 163 177 191	60 71 83 95 109 123 138 153 169 186 204 222 241 260	75 89 104 120 137 155 174 194 214 236 258 281 305 330	108 126 146 167 188 211 235 260 287 314 342 371 401	172 196 222 249 277 307 338 370 403 437 473	226 256 287 320 354 390 426 465 504 545	326 363 402 442 484 527 572 619
23 24 25			206 221 237	280 301 322	355 382 408	432 464 497	509 547 586	587 631 676	667 716 767

The values in our *TABLE 5* (Scribner board-foot volumes) are larger than those in *TABLE 1* of Gevorkiantz and Olsen for DBH's of 9 and 10 inches. The values in our table are smaller for lower merchantable heights and larger for higher merchantable heights for DBH's from 11 to 20 inches. The merchantable height where the values in our table become larger increases as DBH increases. For DBH's larger than 20 inches, our table, in general, gives smaller values. In comparing the two sets of tables, it should be kept in mind that our tables assume a 0.5-ft. stump, a minimum top diameter as close as possible to but no smaller than 7.6 inches, and log lengths of 8 ft., whereas the tables of Gevorkiantz and Olsen assume a 1.0-ft. stump, a minimum top diameter that is variable, is no smaller than 8.0 in., and can be considerably larger than 8.0 inches, and log lengths of 16 ft.

Our *TABLES 4* and 5 yield larger values than *TABLES 10* and 6, respectively, of Edminster et al. (1982) except for small merchantable heights. It should be kept in mind that the tables of Edminster et al. assume a 1.0-ft. stump, a minimum top diameter of 5.6 inches, and log lengths of 16 and 8 ft.

## Predicting One Type of Volume from Another

Multiple linear regression equations were developed to predict one type of volume from another using the 750 trees in the prediction data set. Equations were developed for predicting cubic-foot volume (CV) as a function of Doyle (DV), International 1/4-inch (IV), and Scribner (SV), DV as a function of CV, IV, and SV, IV as a function of CV, DV, and SV, and SV as a function of CV, DV, and IV. These equations and their associated  $\mathbb{R}^2$  and  $\mathbb{S}_{V \cdot X}$  values are shown in TABLE 6.

# Predicting Board-foot Cubic-foot Ratios

Doyle (DCR), International 1/4-inch (ICR), and Scribner (SCR) board-foot cubic-foot ratios were calculated for each of the 750 trees in the prediction data set. Average board-foot cubic-foot ratios were 2.88 (range: 1.84 to 4.8), 5.21 (range: 3.85 to 6.32), and

TABLE 6. Regression equations for predicting cubic-foot (CV) and Doyle (DV), International 1/4-inch (IV), and Scribner (SV) board-foot volumes from the other three types of volumes.

Regression Equation	R <sup>2</sup>	s <sub>y•x</sub>
$C_{\text{V}}^{\hat{A}} = 1.5015 + 0.3057 \text{DV} - 0.000443 \text{DV}^2$	0.993	0.66
$C_{X}^{A} = 0.5318 + 0.1853 \text{ IV} - 0.000082 \text{ IV}^{2}$	0.998	0.38
$\stackrel{\wedge}{\text{CV}} = 0.6617 + 0.1955 \text{SV} - 0.000107 \text{SV}^2$	0.998	0.40
$D_{N}^{\wedge}$ = -2.2163 + 2.6741 CV + 0.038958 CV <sup>2</sup>	0.995	2.37
$D_{N}^{\uparrow} = -1.7112 + 0.5443 \text{ IV} + 0.000692 \text{ IV}^{2}$	0.997	1.65
$DV = -1.5017 + 0.5835 SV + 0.000645 SV^2$	0.998	1.41
$\vec{I}_{N}^{A} = -2.2678 + 5.2628 \text{CV} + 0.018523 \text{CV}^{2}$	0.998	2.48
$\vec{I}$ V = 4.7326 + 1.6969 DV - 0.001770 DV <sup>2</sup>	0.997	2.93
$\vec{IV} = 0.6249 + 1.0591 \text{SV} - 0.000123 \text{SV}^2$	1.000	0.43
$\mathring{S}_{A}^{V} = -2.5708 + 4.9298  \text{CV} + 0.022232  \text{CV}^2$	0.998	2.26
$\hat{S}V = 3.7357 + 1.6135  \text{DV} - 0.001518  \text{DV}^2$	0.998	2.16
$SV = -0.5643 + 0.9430  IV + 0.000114  IV^2$	1.000	0.37

4.88 (range: 3.54 to 6.16) for Doyle, International 1/4-inch, and Scribner board-foot volumes, respectively.

Multiple linear regression equations were developed to predict the three types of board-foot cubic-foot ratios as a function of D, H, and D and H. These equations and their associated values of  $\mathbb{R}^2$  and  $\mathbb{S}_{y \cdot x}$  are shown in *TABLE 7*.

Board-foot cubic-foot ratios for the three types of board-foot volume as a function of H are shown in *TABLE 8*. Board-foot cubic-foot ratios for the three types of board-foot volume as a function of D are shown in *TABLE 9*.

#### Validation

The data set used to validate the prediction equations consisted of 196 trees, the remaining approximately 20% of the total of 946 trees. For each volume equation, the average relative error as a percent  $(\overline{RE})$  was calculated where

$$\overline{RE} = \sum_{i=1}^{n} RE_i/n$$

and  $RE_i = [(\hat{V}_i - V_i)/V_i] \times 100$ ,  $\hat{V}_i$  and  $V_i$  are are the predicted and actual volumes for the  $i\frac{th}{t}$  tree, and n is the number of trees in the validation data set (n = 196). The relative error as a percent for the sum of the predicted volumes was also calculated where

$$RE_{S} = \begin{bmatrix} n & n & n \\ (\sum V_{i} - \sum V_{i}) / \sum V_{i} \\ i = 1 & i = 1 \end{bmatrix} \times 100$$

and  $\sum_{i=1}^{n} \hat{V}_{i}$  and  $\sum_{i=1}^{n} V_{i}$  are the sum of the predicted and actual volumes, respectively.

TABLE 7. Regression equations for predicting Doyle (DCR), International 1/4-inch (ICR), and Scribner (SCR) board-foot cubic-foot ratios as in function of D, H, and D and H.

Type of Ratio	Regression Equation	$\mathbb{R}^2$	s <sub>y•x</sub>
	$D_{CR}^{\wedge} = -0.351 + 0.300D$	0.829	0.20
Doyle	$\overrightarrow{DCR} = 2.006 + 0.310H$	0.787	0.23
·	$\overrightarrow{DCR} = 0.471 + 0.187D + 0.138H$	0.868	0.18
	ICR = 3.269 + 0.180D	0.501	0.30
International 1/4-inch	ICR = 4.587 + 0.221H	0.668	0.24
,	$\stackrel{\wedge}{\text{ICR}}$ = 4.587 - 0.000005D + 0.221H	0.668	0.24
	Λ		
	SCR = 2.562 + 0.215D	0.597	0.26
Scribner	SCR = 4.176 + 0.251H	0.719	0.22
	SCR = 3.827 + 0.043D + 0.212H	0.725	0.22

TABLE 8. Predicted Doyle (DCR), International 1/4-inch (ICR), and Scribner (SCR) board-foot cubic-foot ratios as a function of H.

Н	Board-fo	ot Cubic-foot Ra	atio
(Sticks)	DCR	ICR	SCR
1 2 3 4 5 6 7 8 9	2.3 2.6 2.9 3.2 3.6 3.9 4.2 4.5 4.8 5.1	4.8 5.0 5.2 5.5 5.7 5.9 6.1 6.4 6.6 6.8	4.4 4.7 4.9 5.2 5.4 5.7 5.9 6.2 6.4 6.7

TABLE 9. Predicted Doyle (DCR), International 1/4-inch (ICR), and Scribner (SCR) board-foot cubic-foot ratios as a function of D.

D	Board-foot Cubic-foot Ratio					
(Inches)	DCR	ICR	SCR			
9 10	2.3	4.9	4.5			
10	2.6 2.9	5.1 5.2	4.7 4.9			
12	3.2	5.4	5.1			
13	3.5	5.6	5.4			
14	3.8	5.8	5.6			
15	4.1	6.0	5.8			
16	4.4	6.1	6.0			
17	4.7	6.3	6.2			
18	5.0	6.5	6.4			
19	5.3	6.7	6.7			
20 21	5.6	6.9	6.9			
22	5.9 6.2	7.0 7.2	7.1 7.3			
23	6.5	7.2 7.4	7.5 7.5			
23 24	6.8	7.4 7.6	7.3 7.7			
25	7.1	7.8 7.8	7.7			

For the validation data set, average DBH = 10.8 in. (range: 8.4 to 15.3), average merchantable height = 2.8 sticks (range: 1 to 6), average cubic-foot volume = 12.20 (range: 2.78 to 37.53), average Doyle board-foot volume = 38.90(6.48 to 155.4), average International 1/8-inch. board-foot volume = 72.98 (range: 15.99 to 246.17), and average Scribner board-foot volume = 62.48 (range: 13.14 to 215.48).

TABLE 10 shows RE, range of RE<sub>i</sub>, and RE<sub>s</sub> for the cubic-foot and Doyle, International 1/8-inch, and Scribner board-foot prediction equations.

TABLE 10. Average relative error (RE), range of  $RE_i$ , and relative error for the sum of the predicted values  $(RE_s)$  for the four volume prediction equations (equations 1-4).

Prediction Equation	RE	Range of RE <sub>i</sub>	RE <sub>s</sub>
(1) Cubic-foot	0.9	-14.8 to 21.2	0.23
(2) Doyle	1.7	-21.5 to 24.6	-0.15
(3) International 1/8-inch	1.1	-16.6 to 16.5	0.13
(4) Scribner	1.1	-17.3 to 17.5	-0.013

RE was less than 2% and  $|RE_s|$  was less than 0.25% for all volume prediction equations. Plots of  $RE_i$  versus  $V_i$  showed no prediction problems for the range of  $V_i$ 's in the validation data set except for small values of  $V_i$ . The volume prediction equations over-predict volume for cubic-foot volumes less than 4 and Doyle, International 1/4-inch and Scribner board-foot volumes less than 15, 20, and 15, respectively.

## **Guidelines for Users**

We recommend the use of Equations 1-4 for estimating individual tree volume for aspen in Michigan for most cruising situations. The merchantability limits assumed by these equations closely approximate merchantability limits used by the DNR.

If the user wants to predict one type of volume from another, the appropriate equation in *TABLE 6* can be used. If the user needs to estimate board-foot cubic foot ratios for one of the types of board-foot volumes, the appropriate equation in *TABLE 7* can be used.

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