Geometry Inspection Report prepared for:

Enbridge Energy, Limited Partnership
20"GEMINI™ Geometry Inspection
NPS20 Line 5 North Straits EAST to Mackinaw

Total Distance: 4.13mi

Pipeline Inspection Date: April 17, 2018

Tool Pulled Date: April 17, 2018

Issue Number: J2008-358 Issue #1

Baker Hughes Pipeline Inspection

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Note:

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Information provided herein represents the best efforts of Baker Hughes Pipeline Inspection to evaluate the described lines. Judgements concerning pipe condition are left entirely to Enbridge. All information herein represents only Baker Hughes Pipeline Inspection's opinion of the meaning of the GEMINI™ information, and shall not be construed as a warranty or guarantee of the structural condition of the pipeline, its fitness for use, or any other condition.

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1 EXECUTIVE SUMMARY

Baker Hughes Pipeline Inspection has successfully completed an inertial geometry survey of Enbridge's 4.13mi NPS20 Oil pipeline, running North Straits EAST to Mackinaw. The successful run was performed on April 7, 2018. The purpose of the inspection was to determine pipeline geometry, which includes plan, profile, bends, weld tally, and pipe wall deformations.

The analysis of the caliper data has identified 1 dent greater than 2% O.D. No wrinkles greater than 2% O.D. or ovalities greater than 5% O.D. were found in the line. The dent is 0.67in (3.3% O.D.) located at absolute chainage 8,821.03ft. There are no dents interacting with metal loss anomalies. The complete anomaly listing is included in Appendix 2.

1 internal diameter restriction, where the I.D. was less than 90% O.D., was identified during the caliper analysis. The internal diameter restriction is 17.67in (88.3% O.D.) and located at absolute chainage 8,821.0ft at dent. The internal diameter restriction listing is included in Appendix 3.

The analysis of the inertial data has identified 20 bends with an angle larger than 1.5° and a radius of curvature less than 100D. No bends are tighter than 5D in the line. All bends are listed in Appendix 5.

The line was analyzed for pipeline movements between the current inspection and 2003 GEMINI™ Inspection. The reporting threshold is to report pipeline movements with differential bending strain exceeding 0.1% and spanning over more than one joint. No areas of pipeline movement, except the launcher and receiver replacements, were found meeting the reporting threshold within this line. The areas of pipeline replacement are listed in Appendix 4 and illustrated in Appendix 10.

Enbridge provided updated GPS coordinates in 2016 for 2 locations along the entire line, consisting of the launch and receive valves. Since the 2005 and 2013 GEMINI™ inspections, both the launch and receive areas of the pipeline have been replaced. This information was integrated with the pipe centerline coordinates obtained from the inertial survey, providing a means for locating pipeline anomalies and a foundation for a Geographic Information System (GIS). A listing of the UTM coordinates based on the NAD83 datum is listed in Appendix 1.

One copy of the survey data and the BHI software for viewing is stored on the enclosed DVD. The complete pipeline tally including girth welds, pipe fittings, wall thickness transitions, bends and anomalies can be displayed in BHI's software together with the caliper and inertial data. This information is also available in the Microsoft Excel file "BHI 2018 GEMINI Survey NPS20 Line 5 North Straits EAST - Mackinaw Issue 1.xls", which is located in the directory "\BHI\ NPS20_Line5_North_Straits_EAST-Mackinaw\2018_GEMINI_FINAL REPORT Issue #1 Caliper" on the DVD. Also included on the DVD-ROM is the Enbridge pipeline listing with RPS8.2.

A copy of Enbridge ILI Minimum Reporting Requirements Guide 8.2 is included in Appendix 12.

2 Inspection Summary

2.1 Operational Details

Baker Hughes Pipeline Inspections has mobilized equipment and a qualified crew to perform in-line inspections of the following system:

BHI Job Number	J2008-358
Pipeline Operator	Enbridge Energy, Limited Partnership
Segment Name	Line 5 North Straits EAST - Mackinaw
Launch Site	Ignace, Michigan
Receive Site	Mackinaw City, Michigan
Pipeline Nominal Diameter	20''
Product	Oil
Section Length	4.13mi
Date of GEMINI™ Inspection	April 17, 2018
Duration of GEMINI™ Inspection	1 hour 57 minutes
Field Project Manager	Dale Simpson

Table 1. Operational Details

After passing all of the Baker Hughes pre-run inspection procedures, the GEMINI™ was launched at 13:16 EDT on April 17, 2018. The tool entered the receive trap at 15:13 EDT on April 17, 2018. The GEMINI™ tool was received relatively clean with 1 damaged Caliper sensor arm.

Field analysis indicated that a 98.24% of caliper data was collected for the run. 1 Caliper sensor arm was damaged after passing a tee at launch. But this didn't affect the sizes of the reported geometry anomalies. All other systems, including Inertial, odometer, pressure and temperature sensors functioned normally for the entire run.

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2.2 Reporting threshold

The reporting criteria are to report

- Dents and wrinkles greater than or equal to 2% of nominal O.D. of the pipeline
- Multi-apex geometric anomalies greater than or equal to 1% O.D.
- Top side geometric anomalies greater than 0.5% O.D. and in close proximity to a dent or geometric anomalies greater or equal than 1% O.D.
- Bottom side geometric anomalies greater than 0.5% O.D. and in close proximity to a dent greater or equal than 2% O.D.
- Ovalities greater than or equal to 5% O.D.
- Areas of pipeline movement with bending strain difference exceeding 0.1% and spanning more than 1 pipe joint

The anomaly size definition varies by feature type and is provided in Section 5.4. Details of the reporting specifications and features definition can be found in Enbridge's Inline Inspection Reporting Profile standard Version 8.2 included in Appendix 13.

3 SURVEY RESULTS

The GEMINI™ inertial survey provides pipeline plan, profile and bending strain, allowing one to locate the pipeline in the GPS mapping projection, and to detect pipeline movement between runs. The positional information is derived from the onboard strapdown inertial unit, the odometer readings and the GPS coordinates of selected tie points obtained from a GPS survey.

The caliper survey provides the information on the internal diameter and shape of the pipe, allowing for detection and measurement of pipe wall anomalies (dents, ovalities and wrinkles), wall thickness changes, valves, tees and girth welds.

3.1 Chainage

The GEMINI™ chainage is the distance measured by the GEMINI's odometers along the pipeline and is denoted as SCh (slack chainage) on the plots. It starts from 33.36ft at the pig launch trap and ends at 21,781.82ft in the receive trap. A separate client chainage that correlates the GEMINI™ slack chainage to the Enbridge's As-built chainage has been created. A one-page sample of the BHI – Enbridge chainage correlation listing is included in Appendix 7. The horizontal chainage is also available, and it represents the true horizontal distance of the surveyed pipeline.

3.2 GPS Tie Points

Enbridge provided updated GPS coordinates in 2016 for 2 locations along the entire line, consisting of the launch and receive valves. Since the 2005 and 2013 GEMINI™ inspections, both the launch and receive areas of the pipeline have been replaced. This information was integrated with the pipe centerline coordinates obtained from the inertial survey, providing a means for locating pipeline anomalies and a foundation for a Geographic Information System (GIS). A listing of the UTM coordinates based on the NAD83 datum is listed in Appendix1.

3.3 Pipe Anomalies

The caliper data was used for detecting and sizing diameter restrictions and pipe wall anomalies, such as ovalities, dents, and wrinkles. The anomaly size definition is provided in Section 5.4.

The analysis of the caliper data has identified 1 dent greater than 2% O.D. No wrinkles greater than 2% O.D. or ovalities greater than 5% O.D. were found in the line. The dent is 0.67in (3.3% O.D.) located at absolute chainage 8,821.03ft. There are no dents interacting with metal loss anomalies. The complete anomaly listing is included in Appendix 2.

Summary of Pipewall Deformations

Deformations		Dents				Ovalities	Inward Wrinkles	Outward Wrinkles
		All (≥ 2%)	≥ 6%	Top of Pipe	Near GWD			
Total Number		1	0	1	0	0	0	0
Largest	Size (%OD)	3.34		3.34				
	Absolute Distance (ft)	8,821.03		8,821.03				

Geometry Feature Severity

Feature Type	Top	Bottom	Max Depth %
Geometry Feature depth d ≥5%	0	0	
Geometry Feature associated with stress risers or welds	0	0	

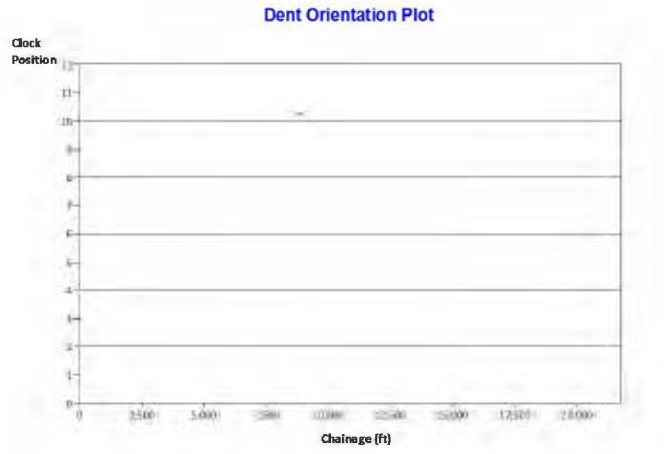
Wrinkle/Buckle Severity

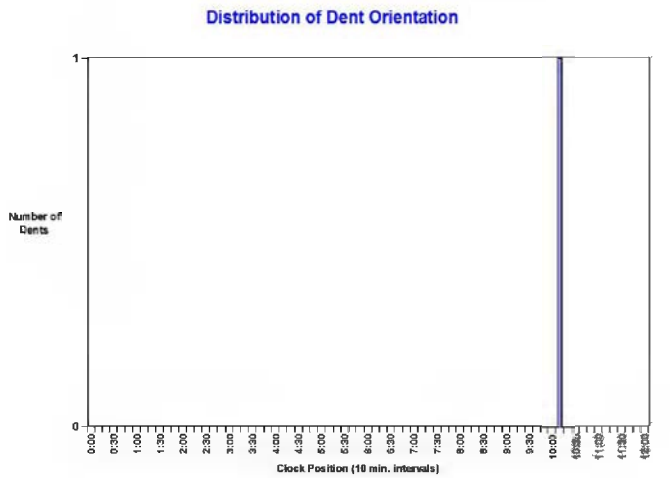
Feature Type	Top	Bottom	Max Depth %
Wrinkles/Buckles	0	0	
Wrinkles/Buckles across seam welds or girth welds	0	0	

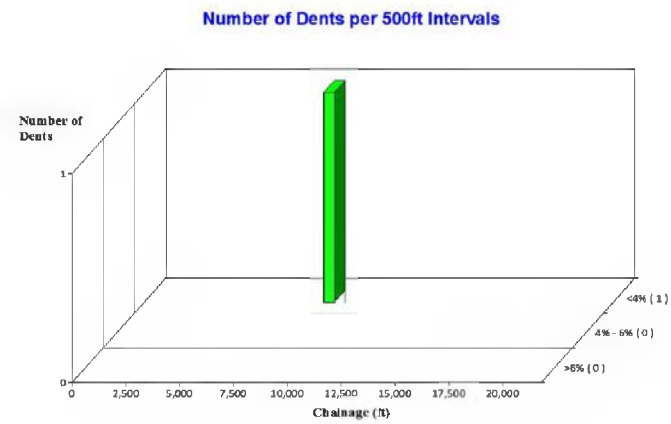
Appendix 12 contains inspection sheets for the dent. There are three inspection sheets per anomaly: a dig sheet showing the position of the feature in a pipe joint together with the adjacent joints, a plot of pipeline plan and profile between the nearest u/s and d/s reference points, and a plot showing 3 views of the anomaly: 3-D view, pipe cross-section and diameter profile. The 3-D view scale is exaggerated 3 times. The pipe diameter profile consists of 25 lines showing the pipe internal diameter at different clock positions measured by the 25 pairs of opposing caliper arms. The clock positions of these caliper arms are colour coded according to the spectrum displayed on the left side of the plot.

1 internal diameter restriction, where the I.D. was less than 90% O.D., was identified during the caliper analysis. The internal diameter restriction is 17.67in (88.3% O.D.) and located at absolute chainage 8,821.0ft at dent. The internal diameter restriction listing is included in Appendix 3.

The following plots show the distribution and orientation of dents along the pipeline.







3.4 Bends

The analysis of the inertial data has identified 20 bends with an angle larger than 1.5° and a radius of curvature less than 100D. No bends are tighter than 5D in the line. All bends are listed in Appendix 5.

3.5 Pipe Movement

The line was analyzed for pipeline movements between the current inspection and 2003 GEMINI™ Inspection. The reporting threshold is to report pipeline movements with differential bending strain exceeding 0.1% and spanning over more than one joint. No areas of pipeline movement, except the launcher and receiver replacements, were found meeting the reporting threshold within this line. The areas of pipeline replacement are listed in Appendix 4 and illustrated in Appendix 10.

Strain Severity

Feature Type	No. of Features	Largest Peak Strain Difference Vertical %	Largest Peak Strain Difference Horizontal %	Largest Peak Strain Difference Total%	GW	Distance (m)	Comments
Pipe Movement	2	N/A	N/A	NA	N/A	N/A	Launch and receive areas replaced since 2005
Largest Movement	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	N/A	N/A	N/A	N/A	N/A	N/A	N/A

Pipe Movement

Feature Type	No. of Features	Vertical Movement (ft)	Horizontal Movement (ft)	GW	Distance (m)	Comments
Pipe Movement	2	N/A	N/A	N/A	N/A	Launch and receive areas replaced since 2005
Largest Movement	N/A	N/A	N/A	N/A	N/A	N/A
	N/A	N/A	N/A	N/A	N/A	N/A

3.6 Pipe Tally

The pipe internal diameter measured by the calipers is used for calculation of pipe wall thickness assuming a constant pipe O.D. The wall thickness transitions were correlated with the listing supplied by Enbridge, and is attached in Appendix 6. The list of valves and tees are included in Appendix 7.

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The GEMINI™ has also detected all the girth welds in the pipeline. They are listed in the worksheet "Weld Log", which contains the information on the length and start chainage of each pipe joint. The weld log combined with all the other features in the pipeline (valves, tees, wall thickness transitions, anomalies and bends) are listed in the worksheet "Pipe Tally". A one-page sample of the pipe tally listing is included in Appendix 9.

All the listings included in Appendices 1 to 9 as well as the full pipe tally are available in electronic form in the MS Excel spreadsheet "BHI 2018 GEMINI Survey NPS20 Line 5 North Straits EAST - Mackinaw Issue 1.xls".

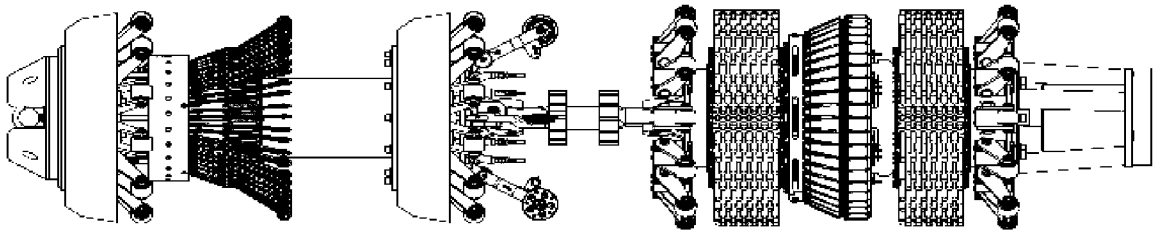
3.7 Plan and Profile

The first plot in Appendix 11 shows the plan, profile, internal diameter and pig velocity, valves, and AGM locations of the entire pipeline. The remaining 6 plots show the pipeline plan, profile, internal diameter and location of selected features, such as valves, tees, anomalies, I.D. restrictions, pipeline movements and wall thickness transitions at 4,000ft per page.

4 GEMINI DESCRIPTION

4.1 System Description

The GEMINI™ is designed to meet a large variety of user requirements using a modular system that integrates a variable number of different sensors. The design of the NPS20 GEMINI™ consists of two pig carriers, as illustrated bellow.



20" Mechanical Caliper GEMINI™

A Strapdown Inertial Navigation System is the heart of the GEMINI™ and delivers position and attitude of the pig along its trajectory within the pipe. Due to the nature of inertial measurements regular "updates" of attitude, position, and velocity are required. External position and attitude are taken from GPS results or alignment sheets.

The GEMINI™ is suspended in the pipeline by urethane disks at front and rear of the carrier. This restricts the GEMINI™ to move close and parallel to the pipe centre line. Mechanical calipers are mounted in the middle of the front carrier and they scan the wall of the pipeline and generate a full picture of the shape of the pipeline. Here the information on dents, ovalities, wrinkles and other features is extracted.

The GEMINI™ is completed by some other sensors and devices: odometers, which measure the distance travelled, tracking transmitter for location of the GEMINI™, and finally, storage device and power supply which allow independent operation for long measurement periods.

4.2 Strapdown Inertial Navigation System

The strapdown INS ultimately produces 3-dimensional measurement of inertial acceleration and angular rate directly from orthogonal triads of accelerometers, and single degree of freedom gyros. In the case of a pair of two degree of freedom gyros, a redundant or combined axis measurement is available, and is dealt with appropriately to produce 3 axis orthogonal angular rates. The strapdown accelerometers and gyros are complementary sensors which when coupled deliver the measurements for computing pipeline curvature, orientation of the curvature, and the positioning capability for location of the curvature or other detected features.

4.3 Caliper

One ring of mechanical calipers scans the wall of the pipe. The caliper arms are spaced at precisely machined constant angles around the ring on the pig. An accurate offset was added to these ranges to give the actual distance from the centre of the carrier to the pipe wall. There are 50 mechanical caliper arms mounted in the middle of the carrier.

4.4 Other Sensors and Components

Other sensors and components integrated in the GEMINI™ are:

- Odometer wheels providing direct measurements of distance traveled (chainage). Velocity is derived from these time tagged distances.
- Temperature and pressure sensors
- A flash memory system
- Interface electronics
- Batteries
- Micro-processor controllers
- Power management module
- Pig Tracking Module (Electromagnetic)

4.5 Survey Accuracy Specifications

The accuracy of the GEMINI™ measurements are as follows:

- Pipeline position 1:2,000
- Bending strain +/- 0.02%
- Bend angle +/- 0.1 °
- Anomaly size +/- 0.1”
- Temperature +/- 0.1 Deg C
- Pressure 0.1% or +/- 3 PSI (0.2 BARSG)

5 DATA ANALYSIS PROCEDURES

The primary function of the GEMINI™ inertial survey is to determine the pipeline plan, profile and bending strain. This is achieved by computing the GEMINI's trajectory during the run using the data collected by the onboard strapdown inertial unit and the odometers. Due to a tight fit of the GEMINI™ cups into the pipe the tool rides practically along the pipe centreline. The only exception from this is the deviation of the tool trajectory from the pipe centerline due to serious pipe wall deformations, as well as "smoothing out the corners" over the transition length (equal to the distance between the cups) at the bend boundaries and at the girth welds exhibiting noticeable out-of-straightness, i.e. sudden change of direction due to the weld misalignment. That data it is then rotated into the GPS co-ordinates of the selected tie-points along the line (usually a few mile apart) to obtain the desired location accuracy in a given UTM mapping projection.

The following paragraphs outline the methods used for processing the odometer and inertial data in order to obtain the pipeline slack and horizontal chainage, client chainage, pipeline position and bending strain.

5.1 Chainage

The following types of chainages are used for referencing the GEMINI™ data:

- slack chainage - the distance measured by the GEMINI's odometers along the pipeline.
- horizontal chainage - the true distance along the pipeline projection on the horizontal plane. Not required by the client in this survey.
- client chainage - the reference system used by the pipeline operator (e.g. station number used on the as-built drawings, or KP location from the ROV survey).

5.1.1 Slack Chainage

The GEMINI™ slack chainage is the distance measured by the GEMINI's odometers along the pipeline. It starts from zero at the reducer on the pig launcher and ends at the receive trap. The odometer accuracy is 0.1 %.

The chainage from the first run is used as the baseline for all the subsequent runs. The preliminary chainage from the subsequent runs derived from the odometer data is scaled to match the distance between the girth welds from the baseline survey. Therefore any change of pipeline length between runs, e.g. elongation due to temperature differential, is disregarded.

5.1.2 Absolute Chainage

The GEMINI™ absolute chainage is the distance along the pipeline corresponding to the upstream edge of defects and the centre of other features, measured from the start of the run. The usage of such distance is as per client specifications.

5.1.3 Horizontal Chainage

The GEMINI™ horizontal chainage represents the true horizontal distance of the surveyed pipeline. It is computed from the slack chainage by projecting it on the horizontal plane first, and then scaling it to match the horizontal distance based on the GPS co-ordinates (Northing and Easting). The scaling is performed between the same tie-points that are used for rotating the inertial survey data into its final position.

5.1.4 Client Chainage

The purpose of a client chainage is to represent any one-dimensional information used by the client, which could be correlated to the slack chainage. Usually the client chainage corresponds to the chainage shown on the as-builts, or to the chainage recorded during another in-line inspection. It can be incorporated into the data at any time after the DVD is issued to the client.

5.2 Pipeline Position

The pipeline position is provided in terms of Northing, Easting and Height as a function of the chainage, in a selected mapping projection (usually UTM) and a specified datum.

5.2.1 Tie Points

Inertial data is translated, rotated and scaled to the "tie points" with known co-ordinates. Those points are typically selected at traps, valves, welds, bends, wall thickness transitions, or any other pipeline features that can be detected directly or indirectly by the GEMINI™ sensors. The co-ordinates of those points are usually obtained from GPS survey.

This procedure provides correction for long term drifts that can introduce an absolute position error in the inertial survey over time. By transforming the GEMINI™ trajectory into the tie points, the Northing, Easting, and Height are obtained for any point along the pipe.

The specified accuracy of the inertial survey is 1:2,000 of the distance from the tie points; therefore for the following sample distances between the tie points the following absolute accuracy is obtained:

Distance Between Tie Points [m]	Absolute Accuracy [m]
20,000	5.0
10,000	2.5
5,000	1.25
3,000	0.75

For example, if the data from two GEMINI™ run have been tied to the points that are 3km apart, then the allowable error in-between the ties points can reach 0.75m, which corresponds to up to 1.5m difference between two runs. To reduce the relative difference between two runs, a procedure described in the next section is applied, which ensures that the actual pipeline movement is measured with centimeter accuracy. There is practically no difference in the pipeline position between the runs in the areas where the pipeline did not move.

5.2.2 Pipeline Movement

Once preliminary processing has been completed, the data from the current and the previous GEMINI™ surveys are compared in order to identify the areas of strain differences associated with the pipeline movement. Then the current data is reprocessed using the coordinates of the tie points extracted from the baseline GEMINI™ survey at 100m intervals, except for the previously determined pipeline movement areas. This procedure improves the accuracy of the local pipeline movement measurement by reducing the relative error between two runs. A noticeable error would result from the absolute position accumulation

error when only the original tie points (from the GPS survey, at about 1km spacing) were used for scaling and rotating the inertial survey data.

5.3 Bending Strain

The bending strain is computed directly from the curvature of the GEMINI™ trajectory, typically averaged over the distance of three pipe diameters. The specification for the bending strain measurements from the GEMINI™ survey is +/- 0.02% strain. When the strain difference between two runs is compared that specification is usually exceeded in the originally straight sections of the line, and the accuracy of +/- 0.005% strain is achieved. The following subsections contain the description of the bending strain measurement and general remarks on interpretation of strain data.

5.3.1 Computation Method

There are two main components of the strain tensor in a pipe wall: the longitudinal strain (in the direction of the pipe axis) and the hoop strain (in the circumferential direction). The longitudinal strain is further separated into the axial component and the bending component that changes linearly along the pipe cross-section (see Figure 5.1).

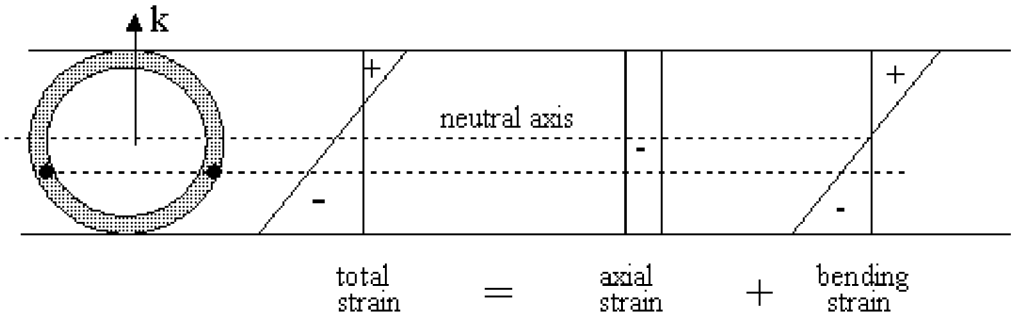


Figure 5.1 Distribution of Axial and Bending Components of Longitudinal Strain in Pipe Cross-section

The bending component of the longitudinal strain at any location in the pipe cross-section can be computed based on the bending strain at two points, e.g. at the top of the pipe (0 o'clock position) and on a right side (3 o'clock position). The bending strain at the bottom of the pipe is called the vertical strain ε_v, because it is induced by bending in the vertical plane (the bending strain at the top of the pipe has the same absolute value, but the opposite sign, i.e. $-\varepsilon_v$). For a similar reason the bending strain on the right side of the pipe is called the horizontal bending strain ε_H (the bending strain on the left side is equal to $-\varepsilon_H$). The maximum bending strain ε in the entire pipe-cross-section is equal to:

$$\varepsilon = \sqrt{\varepsilon_v^2 + \varepsilon_h^2} \,. \qquad (5.1)$$

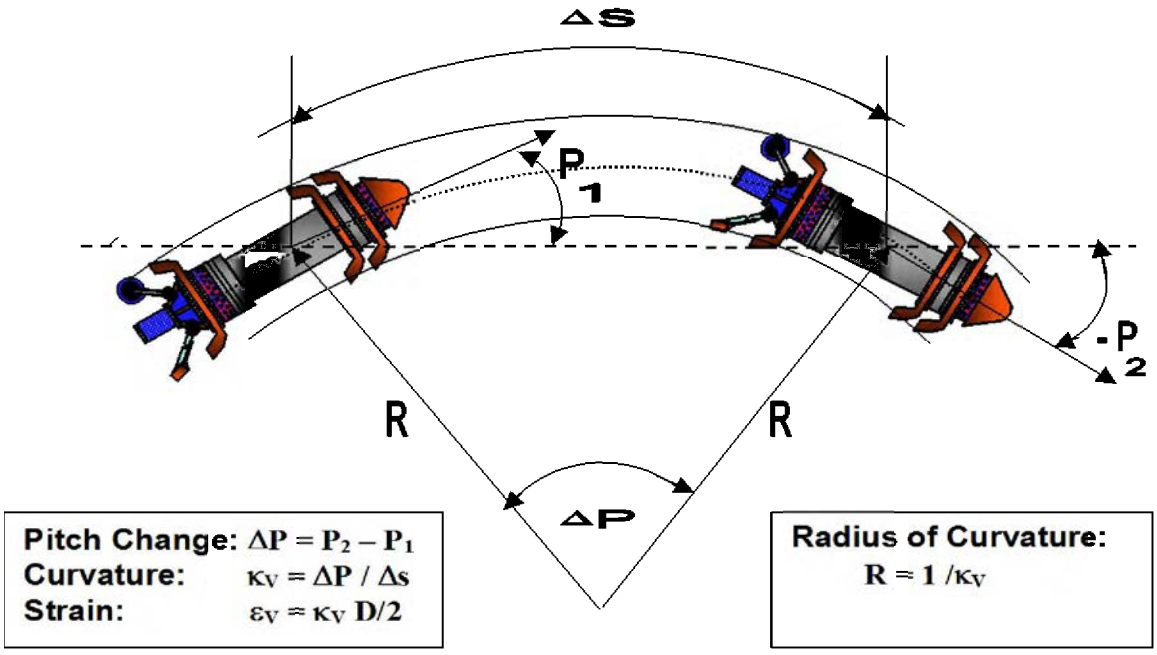


Figure 5.2 Computation of Pipeline Vertical Curvature and Strain from GEMINI Pitch

Both the vertical and horizontal bending strains are computed from the GEMINI™ survey using the measurements of the pipe centerline curvature. The curvature of a line in a 3-D space is defined as the change of direction (in radians) over the distance. The distance is measured by the odometers, and the direction of the pipe centerline is computed from the inertial system in terms of azimuth and pitch. The pitch P(s) describes the pipeline tilt with respect to the horizontal plane at chainage s, while the azimuth A(s) specifies the angle between the pipe direction and the north. The horizontal component of the curvature is proportional to the change of the azimuth, and the vertical component is proportional to the change of pitch. The following formulas are used for computation of the pipeline total curvature κ and its vertical κ_V and horizontal κ_h components based on the changes ΔP and ΔA of pitch and azimuth over a distance Δs along the pipe centerline:

$$\kappa = \sqrt{\kappa_v^2 + \kappa_h^2}\,, \qquad \kappa_v = \frac{\Delta P}{\Delta s}\,, \qquad \kappa_h = -\frac{\Delta A}{\Delta s}\cos(P) \qquad (5.2)$$

The relationship between curvature and bending strain is as follows:

$$\varepsilon = \frac{D}{2}\kappa \qquad \varepsilon_v = \frac{D}{2}\kappa_v \qquad \varepsilon_h = \frac{D}{2}\kappa_h \qquad (5.3)$$

where D is the pipe outside diameter.

The curvature radius is the inverse of the curvature. The BHI software reports strain in percents and the radius of curvature in pipe diameters. Strain is a unitless value that can be expressed in percents by multiplying it by 100%; e.g. 0.45% corresponds to 0.0045 strain.

5.3.2 Smoothing Curvature Data

The curvature can be computed according to formula (5.2) using the change of azimuth or pitch over the chainage increment as small as the distance between two inertial samples. The inertial data is collected at the rate of 100 samples per second. If the tool travels at the speed of 2 m/s then the distance between two samples is only 2 cm. The raw curvature computed this way would exhibit a significant level of noise, e.g. due to tool vibrations. In order to reduce that noise the curvature is typically averaged over a distance of 3 – 5 pipe diameters, i.e. 2-3m for 16" diameter pipe. For computational efficiency, instead of calculating the actual average, the curvature is computed using formula (5.2), where the increments ΔP and ΔA of pitch and azimuth are taken over a distance of 2m. This is practically equivalent to averaging curvature over the same distance - if the data are equally spaced, i.e. when the tool velocity is stable. The longer is the averaging length the smoother are the results.

Another smoothing technique is a regression line fit to the pitch or azimuth considered as functions of chainage. That method fits a line to all of the pitch values (or azimuth) over a specified length. This is practically equivalent to fitting a circle to all of the points along the GEMINI™ trajectory over the specified length, but again much more computationally efficient than actually doing it. The radius of that circle is equal to the radius of curvature of the pipeline. The regression line fit produces smoother results than a regular moving average applied over the same length.

When estimating the bending strain induced by pipe-soil interaction, the curvature can be smoothed out over a length longer than 5 pipe diameters, usually over 5 - 10m. This approach significantly reduces the effect of weld misalignment, pipe wall imperfections and tool dynamics on the computed curvature, and at the same time it doesn't underestimate the bending strain induced by pipeline movement. This approach is particularly suited for calculation of strain difference between two runs. However, averaging over too long distance is not proper for computation of curvature of short features, such as bends or buckles. The bending strain of a feature would be underestimated if the feature was shorter than the effective averaging distance, which includes both the length used in curvature computation and the tool length, i.e. the distance between the cups supporting the pig body (i.e. the inertial canister in case of multi-body tools).

5.3.3 Interpretation of Bending Strain Data

The GEMINI™ measures the total pipeline bending strain at the time of inspection, which includes strain induced during manufacturing, construction and operation. While pipeline is in operation the strain may be caused by the operating conditions (temperature and pressure differential) or by the external forces affecting the pipeline as the results of sea-bottom scouring, sub-sea currents, slope instability, soil settlement and erosion, etc. As the GEMINI™ measures the total bending strain, including the plastic component induced during the whole history of loading, the current shape of the pipe and its bending strain cannot be fully explained by taking into consideration only the forces acting on the pipe during the inspection, e.g. the gravity, buoyancy and support reaction.

The GEMINI™ measures the curvature of the pipe centerline with all its imperfections, including the out-of-straightness at welds that is theoretically described by infinite curvature, although it does not correspond to any bending strain in the pipe wall. When such curvature is measured by the GEMINI™ is obviously not infinite due to the finite length of the tool and some additional smoothing applied during data processing, but it may still show up as spikes of significant amplitude in the curvature data.

When analyzing the bending strain induced during operation the high residual plastic strain present in the field bends should be disregarded. The main features distinguishing the bending strain induced during operation from the field bends are briefly discussed below. The bending strain in the field bends is usually in the range from 1 to 2% strain and is confined to one pipe joint and is characterized by an abrupt change of strain at the beginning and the end of a bend. The bending strain induced during operation is usually of smaller amplitude, spans more than one pipe joint and undergoes gradual change over longer transition sections.

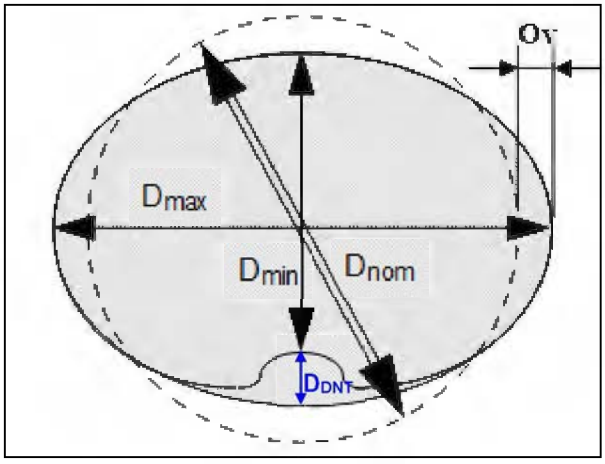
ENBDNR0005725

5.4 Pipewall Anomaly Calculation

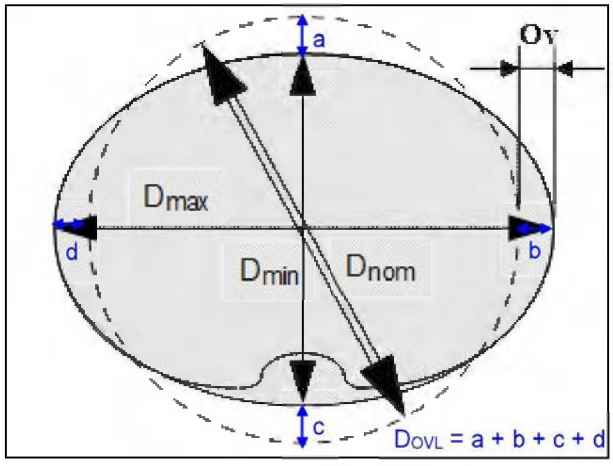
The caliper information is processed to provide the internal shape and diameter of the pipeline. The anomaly size D (depth) is calculated as follows:

For dents: $D_{DNT} = D_{Rstr} - 2*O_V$ without ovality $D_{Rstr} = D_{Nom} - D_{Min}$

$O_V = (D_{Max} - D_{Nom})/2$



For Ovality: $D_{OVL} = D_{Max} - D_{Min}$ CSA Z662



where:

D_{Rstr} - total diameter restriction
O_V - pipe ovality
D_{Nom} - inner nominal pipe diameter
D_{Min} - inner pipe diameter at the feature
D_{Max} - inner pipe diameter 90° from the feature

The dent length and width are calculated as the axial distance and the circumferential distance between points of zero radial deflection respectively. The ovality length and width are calculated as the axial distance and the circumferential distance over which the feature depth exceeds 50% of its peak value respectively. A dent with the width larger than its length

is called an inward wrinkle. The outward wrinkle is characterized by a local increase of pipe diameter.

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6 BHI Software Installation

The report is accompanied by a DVD-ROM containing the BHI display software and the data from the present survey. The data can be viewed using the GEMINIView and GeoDisplay programs running in Microsoft Windows operating system. GEMINIView is used to display the 3-D view of the pipe and the inner pipe wall shape measured by the calipers. GeoDisplay is used for displaying the inertial, odometer, weld, caliper, and other data bases (if available).

The directory structure on the DVD is as follows:

\BHI\NPS20_Line_5_North_Straits_EAST_Mackinaw \2018_GEMINI, which contains:

- several subdirectories with the GEMINI™ data from the run
- environment file 2018_GEMINI_Geometry_NPS20_Line5_North_Straints_EAST_Mackinaw_Issue1.env with the information on the location of the data files from the run. (%RootDir% specifies the path, and %BaseName% - the name)

\BHI\BHI_Software with the software stored on two subdirectories:
\GEMINIView with the GEMINIView program (GEMINIVIEW.EXE)

The entire content of the DVD can be copied to a network drive, or a local hard drive for faster access of the data and the ability to save configurations files with customized displays. The programs can be also stored on the local hard drive while the data is accessed from the DVD or a network drive. In this case only the \BHI_Software subdirectory needs to be copied on the local hard drive.

GEMINIview:

To setup the GEMINIView program for the first time on a computer:

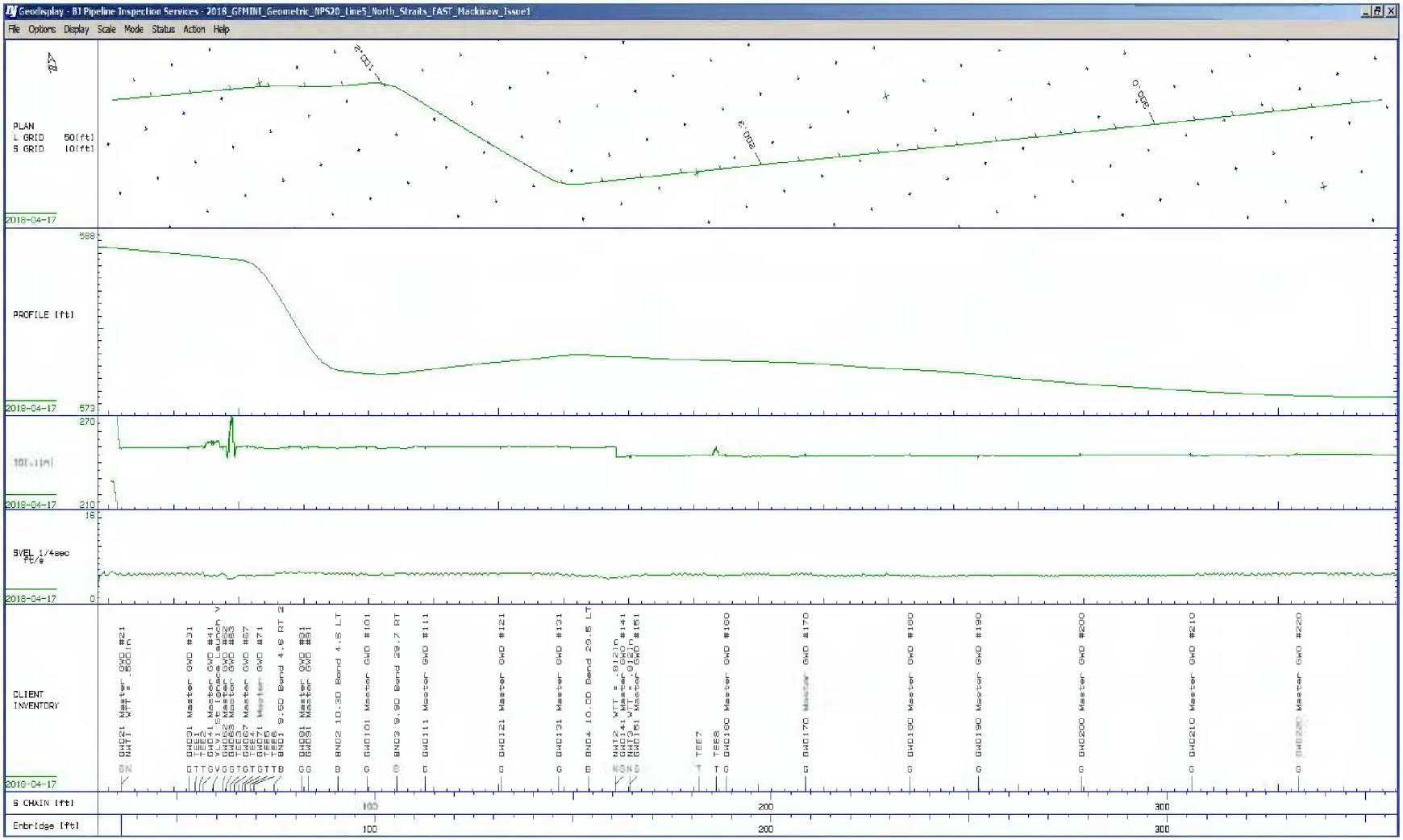
- Run the setup.exe program in the BHI\BHI_Software\GEMINIView directory.

To launch the GEMINIView program:

- Double click GEMINIview_3.21.0.0.exe

Jobs can then be loaded using the File ⇒ Open menu

Appendix 9. Pipe Tally – Sample Plot



Appendix 11. Plots of Pipeline Plan, Profile, Internal Diameter and Features